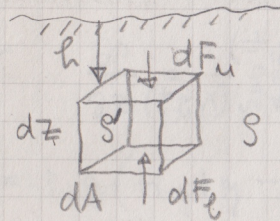


Internal gravity waves

Buoyancy force

I)



$dF_u = \rho g h dA$ (Archimed.)

$dF_e = \rho g (h + dz) dA$

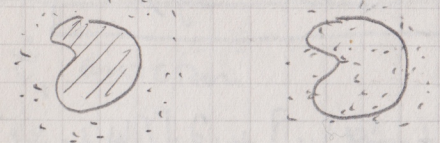
$dF_b = dF_u - dF_e$
 $= -\rho g dz dA$

$g_b = \frac{dF_b}{dm} = - \frac{\rho dV}{\rho' dV} g = - \frac{\rho}{\rho'} g$

if $\rho = \rho'$ then $g_b = -g$: equilibrium

if $\rho' < \rho$ then $\begin{matrix} \uparrow g_b \\ \downarrow g \end{matrix}$: body is driven upward

II) Archimedisches Prinzip



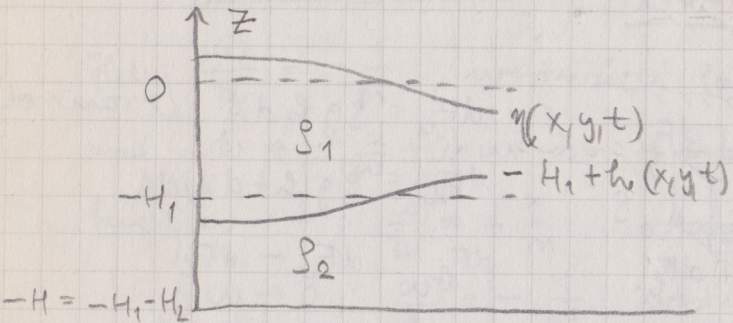
PE in Water Water in Water

the same F_e , since it is caused by outer water & doesn't know body interior.

Two superimposed layers
with internal gravity waves

A. Eijl

use shallow water theory! Stokes 1847



$$p_1 = \rho_1 g (\eta - z) \text{ aus } \frac{\partial p}{\partial z} = -\rho g$$

Kontinuitätsgleichungen

unten $\frac{\partial h}{\partial t} + \frac{\partial}{\partial x} \left[(H_2 + h) u_2 \right] + \frac{\partial}{\partial y} \left[(H_2 + h) v_2 \right] = 0$
klein klein

$$\frac{\partial h}{\partial t} + H_2 \left(\frac{\partial u_2}{\partial x} + \frac{\partial v_2}{\partial y} \right) = 0 \quad \mathcal{L}_2$$

oben $\frac{\partial}{\partial t} (\eta - h) + \frac{\partial}{\partial x} \left[(H_1 + \eta - h) u_1 \right] + \frac{\partial}{\partial y} \left[(H_1 + \eta - h) v_1 \right] = 0$
klein klein

$$\frac{\partial}{\partial t} (\eta - h) + H_1 \left(\frac{\partial u_1}{\partial x} + \frac{\partial v_1}{\partial y} \right) = 0 \quad \mathcal{L}_1$$

Gleichungen

oben

$$\frac{\partial u_1}{\partial t} = -g \frac{\partial \eta}{\partial x}$$

$$\frac{\partial v_1}{\partial t} = -g \frac{\partial \eta}{\partial y}$$

\mathcal{E}_1

unten

$$\frac{\partial p}{\partial z} = -\rho g \rightarrow \Delta p = -\rho g \Delta z$$

$$p_2 = \rho_1 g (H_1 + \eta - h)$$

+ $\rho_2 g (-H_1 + h - z)$ einsetzen in

$$\frac{\partial u_2}{\partial t} = -\frac{1}{\rho_2} \frac{\partial p_2}{\partial x} \text{ gibt}$$

$$\frac{\partial u_2}{\partial t} = -\frac{\rho_1}{\rho_2} g \frac{\partial \eta}{\partial x} - \frac{\rho_2 - \rho_1}{\rho_2} g \frac{\partial h}{\partial x}$$

$$\frac{\partial v_2}{\partial t} = -\frac{\rho_1}{\rho_2} g \frac{\partial \eta}{\partial y} - \frac{\rho_2 - \rho_1}{\rho_2} g \frac{\partial h}{\partial y}$$

\mathcal{E}_2

\mathcal{E}_1 in \mathcal{E}_1 einsetzen

$$\frac{\partial^2}{\partial t^2} (\eta - h) + H_1 \left(-g \frac{\partial^2 \eta}{\partial x^2} - g \frac{\partial^2 \eta}{\partial y^2} \right) = 0$$

$$\otimes \frac{\partial^2}{\partial t^2} (\eta - h) - g H_1 \Delta_h \eta = 0 \quad \Delta_h = \partial_x^2 + \partial_y^2$$

\mathcal{E}_2 in \mathcal{E}_2 einsetzen

$$\frac{\partial^2 h}{\partial t^2} + H_2 \left(-\frac{\rho_1}{\rho_2} g \frac{\partial^2 \eta}{\partial x^2} - \frac{\rho_2 - \rho_1}{\rho_2} g \frac{\partial^2 h}{\partial x^2} - \frac{\rho_1}{\rho_2} g \frac{\partial^2 \eta}{\partial y^2} - \frac{\rho_2 - \rho_1}{\rho_2} g \frac{\partial^2 h}{\partial y^2} \right) = 0$$

$$\boxed{\frac{\partial^2 h}{\partial t^2} - g H_2 \Delta_h \left(\frac{\rho_1}{\rho_2} \eta + \frac{\rho_2 - \rho_1}{\rho_2} h \right) = 0} \quad (**)$$

⊕, ⊕ sind 2. u. 4. Ordnung für $\eta + h$, also
1. u. 2. Ordnung für η

Vereinfachende Annahme: (A) Synchronizität

$$\boxed{h = \mu \eta} \quad \mu = \text{const}$$

$$\left. \begin{aligned} \frac{\partial^2}{\partial t^2} \eta - \frac{g H_1}{1 - \mu} \Delta_h \eta &= 0 \\ \frac{\partial^2}{\partial t^2} \eta - \frac{g H_2}{\mu} \Delta_h \left(\frac{\rho_1}{\rho_2} + \frac{\rho_2 - \rho_1}{\rho_2} \mu \right) \eta &= 0 \end{aligned} \right\} \oplus$$

also muss sein

$$\begin{aligned} \frac{g H_1}{1 - \mu} &= \frac{g H_2}{\mu} \left(\frac{\rho_1}{\rho_2} + \mu \frac{\rho_2 - \rho_1}{\rho_2} \right) \\ &= \frac{g H_2}{\mu} \left(\frac{\rho_1 - \rho_2}{\rho_2} + 1 + \mu \frac{\rho_2 - \rho_1}{\rho_2} \right) \quad \text{also} \end{aligned}$$

$$\frac{g H_1}{1 - \mu} = \frac{g H_2}{\mu} \left(1 - (1 - \mu) \alpha \right) \quad \text{mit } \alpha = \frac{\rho_2 - \rho_1}{\rho_2}$$

Einsetzen in ⊕

$$\ddot{\eta} - c^2 \Delta_h \eta = 0 \quad \text{mit } c^2 = \frac{g H_1}{1 - \mu} = \frac{g H_2}{\mu} (1 - (1 - \mu) \alpha)$$

$$\text{eliminiere } \mu: \quad 1 - \mu = \frac{g H_1}{c^2}, \quad \mu = 1 - \frac{g H_1}{c^2}$$

$$\begin{aligned} \text{dann } \left(1 - \frac{g H_1}{c^2} \right) c^2 &= g H_2 \left(1 - \alpha \frac{g H_1}{c^2} \right) \\ c^2 - g (H_1 + H_2) + \alpha g^2 H_1 H_2 / c^2 &= 0 \end{aligned}$$

$$\boxed{c^4 - g H c^2 + \alpha g^2 H_1 H_2 = 0} \quad H = H_1 + H_2$$

$$c^2 = \frac{g H}{2} \pm \frac{g H}{2} \sqrt{1 - 4 \alpha H_1 H_2 / H^2}$$

Für $\alpha \ll 1$:

$$c^2 = \frac{g H}{2} \pm \frac{g H}{2} \mp g H \alpha H_1 H_2 / H^2$$

Normal mode = barotropic, $p = p(\rho)$

$$\boxed{c^2 = g H} \cdot (1 - \alpha H_1 H_2 / H^2)$$



$$\text{und } \frac{\eta}{h} = \frac{1}{\mu} = \frac{1}{1 - g H_1 / c^2} = \frac{1}{1 - \frac{g H_1}{g (H_1 + H_2)}}$$

$$\text{also } \boxed{\frac{\eta}{h} = \frac{H_1 + H_2}{H_2}} = \text{surface gravity wave}$$

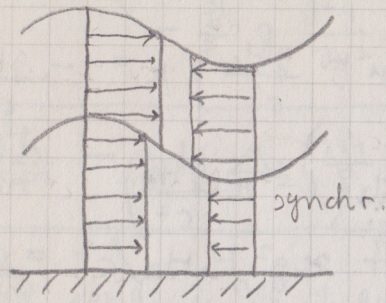
Baroclinic mode

$$\boxed{c^2 = g H \alpha H_1 H_2 / H^2}$$

ist langsam wegen $\alpha \ll 1$.

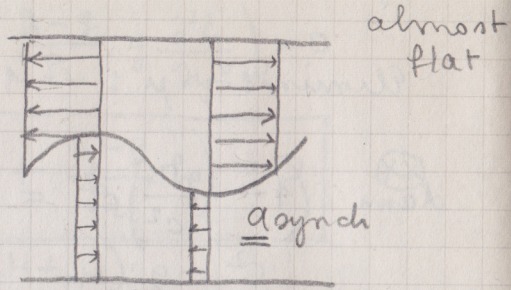
$$\text{und } \frac{\eta}{h} = \frac{1}{\mu} = \frac{1}{1 - \frac{g H_1 H_2}{g H \alpha H_1 H_2}} \approx -\alpha \frac{H_2}{H_1 + H_2}$$

baroclinic mode = internal gravity wave



barotropic surface wave

$$c = \sqrt{gH}$$



baroclinic internal wave

$$c \ll \sqrt{gH}$$

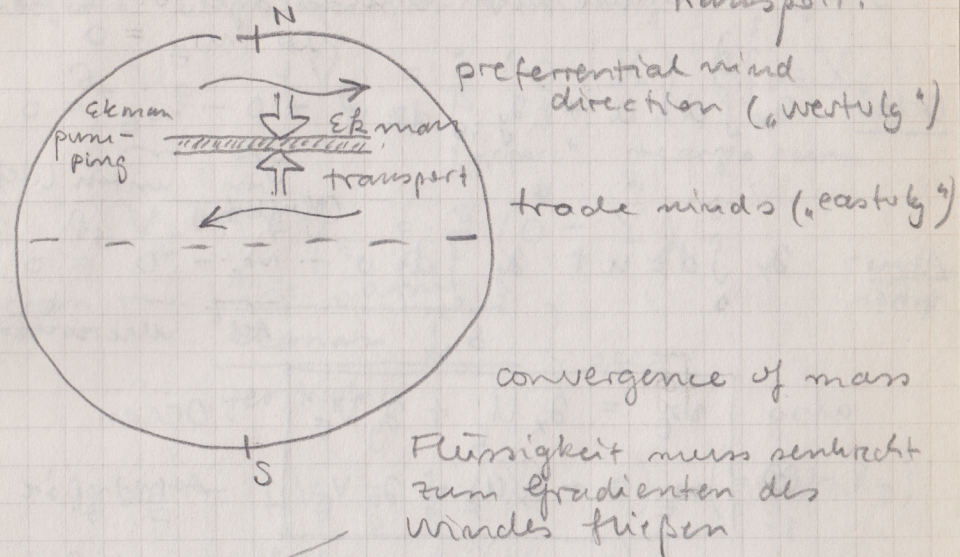
almost flat

Ekman Pumping

7.4.22

Üb 5.326, 327

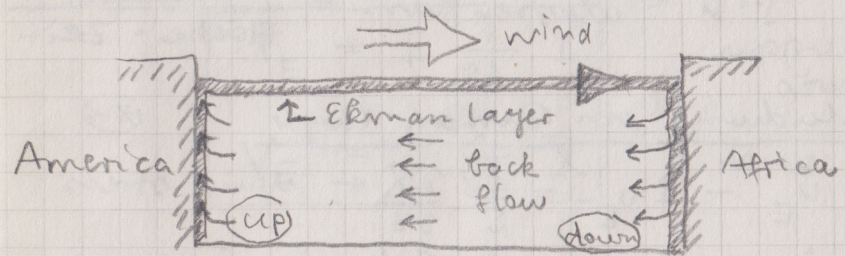
= vertical flow, induced by horizontal Ekman transport.



horizontal ist nicht länger möglich wg. convergence

⇒ vertical transport

Oder so:



= friction dynamics in three thin boundary layers

central result:

$$g w_E = \frac{1}{f} (\partial_x Y - \partial_y X)$$

Kontinuitätsgleichung

$$u_x + v_y + w_z = 0$$

Integriere vertikal durch Ekmanlayer bis Rand
 wo $w_E = 0$

Ocean: $\partial_x \int_{-\delta}^0 dz u + \partial_y \int_{-\delta}^0 dz v + 0 - w_E = 0$

$\underbrace{\hspace{2cm}}_{\text{oben (Oberfläche)}}$ $\underbrace{\hspace{2cm}}_{\text{unten (Tiefsee)}}$

Atmo-sphäre: $\partial_x \int_0^{\delta} dz u + \partial_y \int_0^{\delta} dz v + w_E - 0 = 0$

$\underbrace{\hspace{2cm}}_{\text{"Atm"}}$ $\underbrace{\hspace{2cm}}_{\text{Meeressoberfläche}}$

also $w_E = \partial_x U_E + \partial_y V_E$ Ocean

⊕ $w_E = -\partial_x U_E - \partial_y V_E$ Atmosphäre

mit $U_E = \int dz u$: Massenfluss

denn $\rho \cdot u \cdot A = \frac{\rho g}{m^3} \cdot \frac{m}{s} \cdot m^2 = \text{Masse-strom}$

also $\rho \cdot u = \text{Massenfluss} = \frac{\text{Masse}}{\text{Fläche} \cdot \text{Zeit}}$

Eulergleichung im Ekman layer

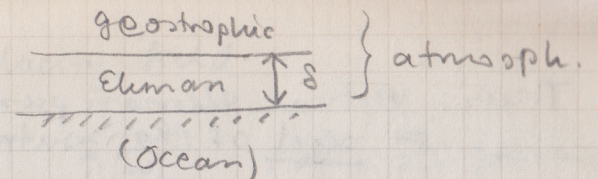
$$\dot{u}_E - f v_E = \frac{1}{\rho} \frac{\partial X}{\partial z} \leftarrow \text{wind stress}$$

$$\dot{v}_E + f u_E = \frac{1}{\rho} \frac{\partial Y}{\partial z}$$

$u_E = v_E = X = Y = 0$ an Unten (Ocean) kante
 Ober (Atmo)

wo geostrophie Strömung

Atmosphäre

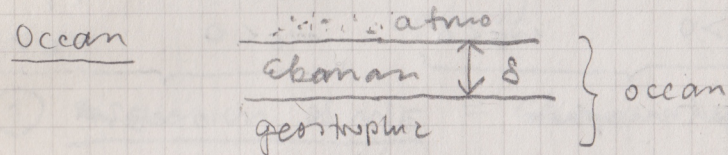


Integrate Euler equation vertically

$$\partial_t U_E - f V_E = \frac{1}{\rho} (0 - X) \left(= \int_0^{\delta} dz X_z \right)$$

\uparrow "space" \uparrow shear on ocean
 \downarrow \downarrow

$$\partial_t V_E + f U_E = \frac{1}{\rho} (0 - Y)$$



$$\partial_t U_E - f V_E = \frac{1}{\rho} (X - 0) \left(= \int_{-\delta}^0 dz X_z \right)$$

$$\partial_t V_E + f U_E = \frac{1}{\rho} (Y - 0)$$

\uparrow ocean surface \uparrow deep down

assume stationary flow

⊗⊗
$$U_E = \mp \frac{1}{\rho f} Y$$

upper sign: atmosphere

lower sign: ocean

$$V_E = \pm \frac{1}{\rho f} X$$

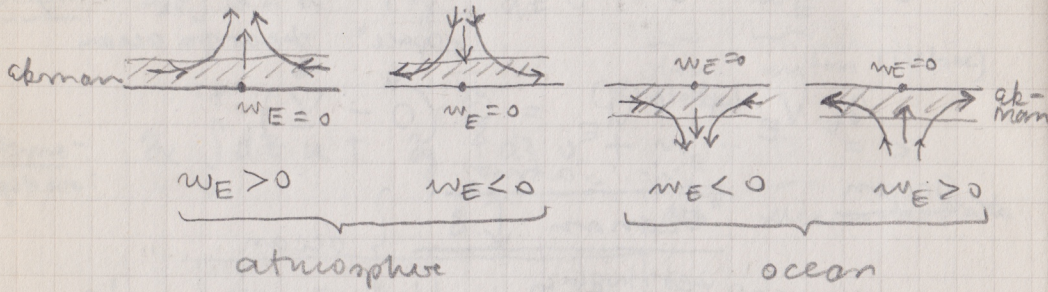
Combine ⊕ & ⊗⊗ with $\rho = \text{const}$, $f = \text{const}$

$$w_E = \frac{1}{\rho f} (\partial_x Y - \partial_y X)$$

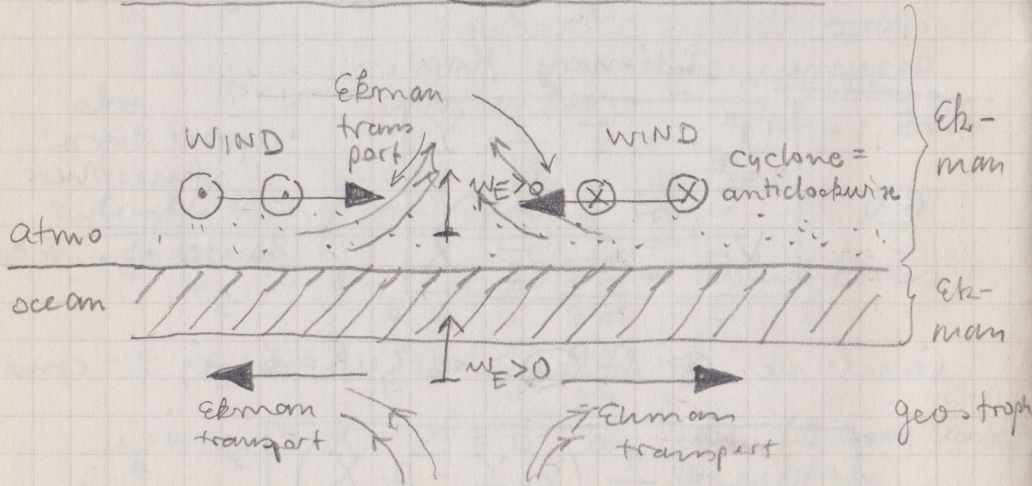
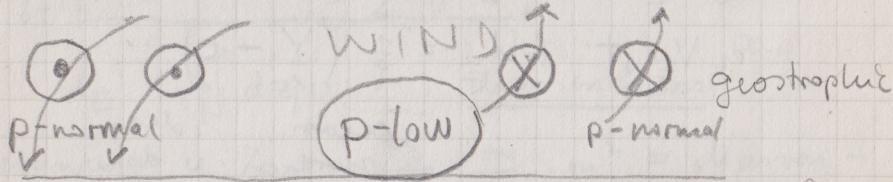
for both ocean & atmosphere! No sign difference

Thus: vertical Ekman pumping
 = curl of (horizontal) wind stress!

again for sign:

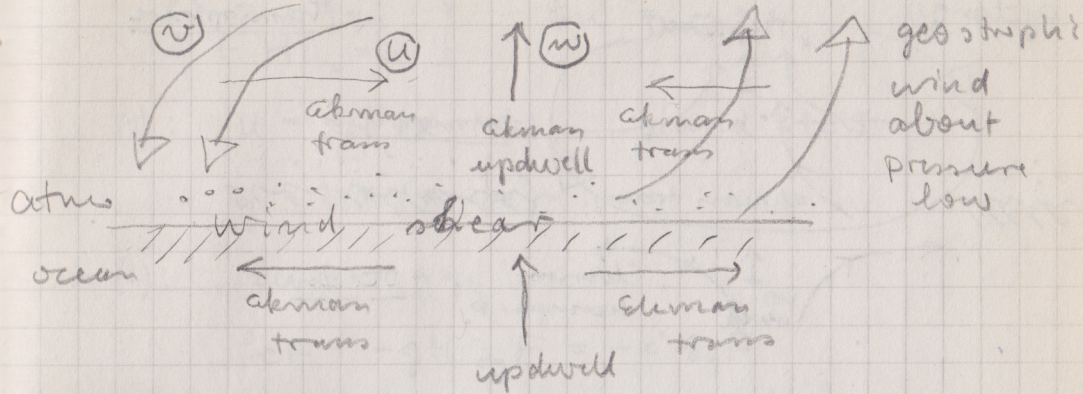


Cyclone over ocean



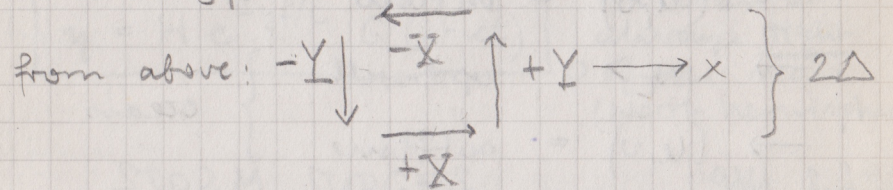
similarly for V_E & X

thus 3-D velocity field



① Discussion of $W_E =$ Ekman upwell

$$W_E = \frac{1}{\rho f} (\partial_x Y - \partial_y X) \text{ atmosph. \& ocean}$$



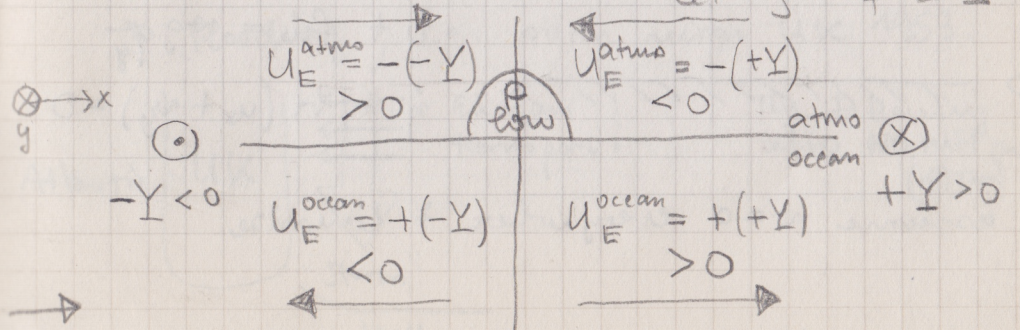
$$\partial_x Y = \frac{Y - (-Y)}{2\Delta} > 0$$

$$\partial_y X = \frac{-X - X}{2\Delta} < 0$$

$$W_E > 0$$

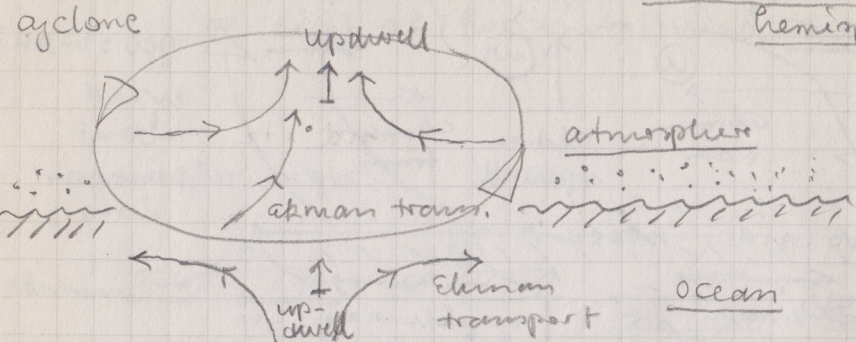
for atmos & ocean

② Discussion of $U_E, V_E =$ Ekman transport
 let $\rho = \rho = 1$



Summary

pressure low over
ocean in north
hemisphere

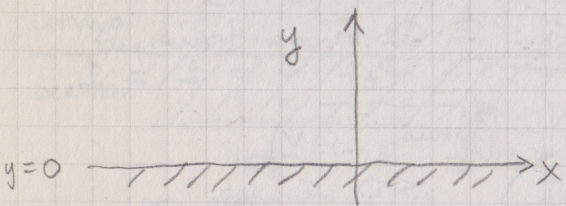


cyclone, positive vorticity

- $w_E > 0$ upwell } atmosphere
- $(u, v) = \text{inflow}$ }
- $w_E > 0$ upwell } ocean
- $(u, v) = \text{outflow}$ }

Remembrance for coming things:

Kelvin wave (Gill chap. 10)



$$\begin{aligned} \dot{u} - fv &= -g\eta_x \\ \dot{v} + fu &= -g\eta_y \\ \dot{\eta} + H(u_x + v_y) &= 0 \end{aligned}$$

assume $v=0$ everywhere & linearize

$$\left. \begin{aligned} \dot{u} &= -g\eta_x \\ fu &= -g\eta_y \\ \dot{\eta} + H u_x &= 0 \end{aligned} \right\} \begin{aligned} \dot{u} - gH u_{xx} &= 0 \quad (1) \\ fu &= -g\eta_y \quad (2) \end{aligned}$$

(1): $u = cF(x-ct)$ (and $x+ct$)

$\eta = HF(x-ct)$

in (2): $fu = -g\eta_y$

$f c F = -gH \partial_y F = -c^2 \partial_y F$

$\frac{dF}{F} = -\frac{f}{c} dy, \quad F = e^{-yf/c}$

$$\begin{aligned} u &= c e^{-yf/c} G(x-ct) \\ \eta &= H e^{-yf/c} G(x-ct) \end{aligned}$$

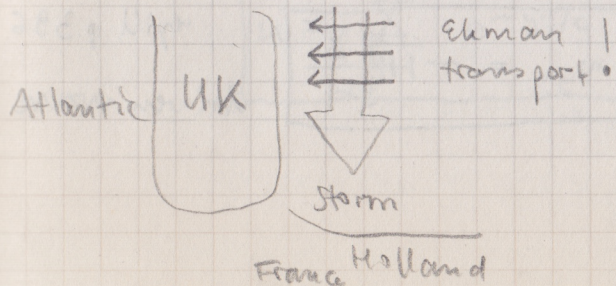
Kelvin wave

The coast is always right of the wave (North hemisphere)

STORM SURGES

Gill p. 395

Summary: a storm along a coast can cause stationary inflow normal to the coast, which causes $\eta \sim t$ of the water surface
→ flooding, e.g. storm surge UK 1953.



The following after NO mit au (1934)

$$\dot{u} - fv = -g\eta_x + \frac{1}{\rho} X_z$$

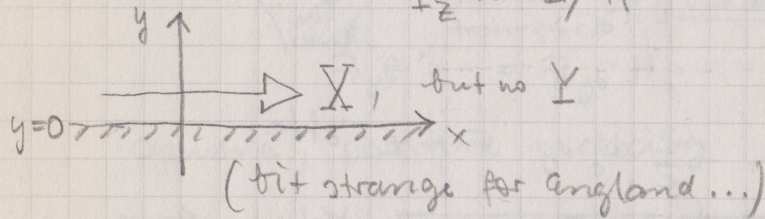
$$\dot{v} + fu = -g\eta_y + \frac{1}{\rho} Y_z$$

$$\dot{\eta} + H(u_x + v_y) = 0$$

Assumptions: $X_z \approx X/H$

$$Y_z \approx Y/H$$

for shallow ocean near a coast



Furthermore: $\partial_x \equiv 0$. Then

$$(1) \quad \dot{u} - fv = X/\rho H \quad \leftarrow \text{Ekman transport}$$

$$(2) \quad \dot{v} + fu = -g\eta_y \quad \leftarrow \text{Kelvin wave}$$

$$(3) \quad \dot{\eta} + H v_y = 0$$

$-f(1) + \partial_t(2) - g\partial_y(3)$ gives

$$-f\dot{u} + f^2v = -f\frac{X}{\rho H}$$

$$+ \ddot{v} + f\dot{u} = -g\dot{\eta}_y$$

$$-g\dot{\eta}_y - gH v_{yy} = 0$$

$$\ddot{v} + f^2v - gH v_{yy} = -\frac{fX}{\rho H} \quad \text{epil p.396 driven wave}$$

Solution is transient wave + stationary part

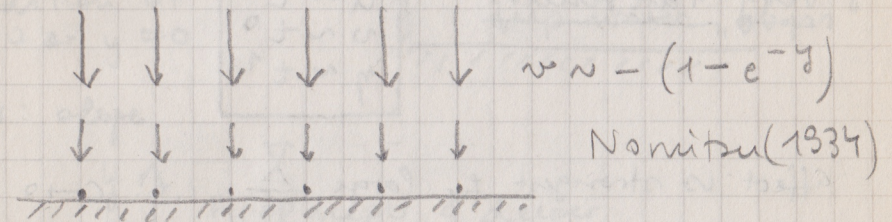
Neglect transient, consider only $\partial_t \equiv 0$

$$f^2v - gH v_{yy} = -\frac{fX}{\rho H}$$

has solution

$$v = -\frac{X}{\rho H} \left(1 - e^{-yf/c}\right) \quad (c^2 = gH)$$

(check is simple)



Continuity: $\dot{\eta} = -H v_y$

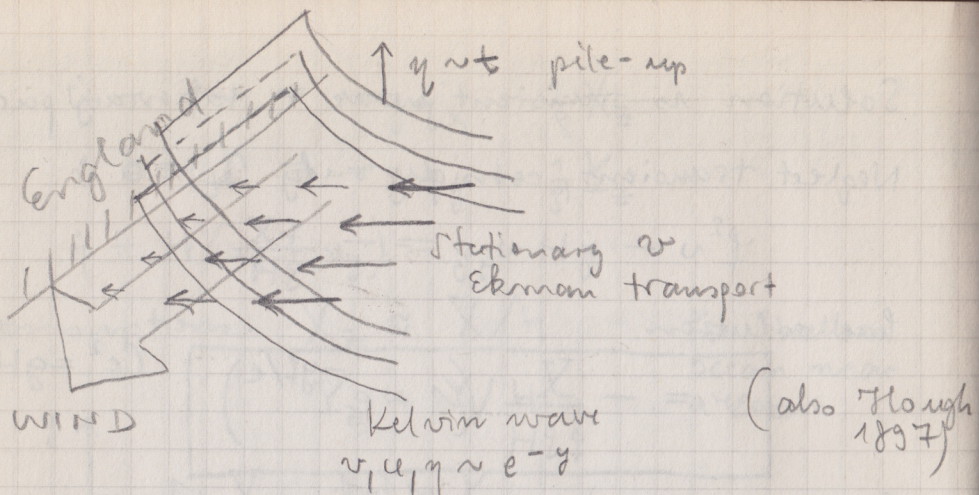
$$= -H \left(-\frac{X}{\rho H c}\right) \left(-\frac{f}{c} e^{-yf/c}\right)$$

$$= +\frac{X}{\rho c} e^{-yf/c}$$

thus $\eta(t) = \frac{X}{\rho c} e^{-yf/c} \cdot t$ linear pile-up!

Euler: $\dot{v} + fu = -g\partial_y\eta$

$$u = \frac{X}{\rho H} e^{-yf/c} \cdot t$$



(also Hough 1897)

very rare result:

$$\begin{cases} u \sim t^1 \\ v \sim t^0 \\ \eta \sim t^1 \end{cases}$$

affect is strongest for large $\frac{X}{gc}$, i.e. $c \rightarrow 0$

ie. $H \rightarrow 0$ Coast

e.g. $H = 50 \text{ m}$, $X = 2 \text{ N/m}^2 \rightarrow$

$d\eta/dt = 1 \text{ m}/3 \text{ h} \hat{=} \text{ storm surge of 1953}$

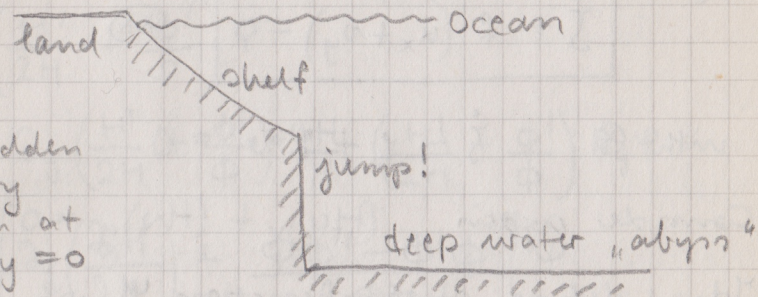
Summary cause for flooding of coast is wind induced Ekman transport

SHELF WAVES

gyll p. 409

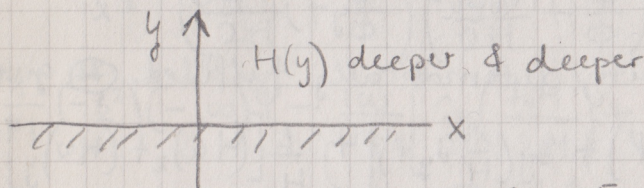
So far $H \approx \text{const}$. Now: strong change in H
Ocean slope near coasts

Shelf:



so far: sudden boundary condition at $x=0$ or $y=0$

Now: slope



Continuity $\dot{\eta} + [(H+\eta)u]_x + [(H+\eta)v]_y = 0$
assumption $\eta \ll H$

$$\dot{\eta} + (Hu)_x + (Hv)_y = 0$$

rigid lid at top: $\dot{\eta} = 0$ (approximation!)

& with $H = H(y)$ alone

$$\boxed{u_x + v_y = -\frac{H_y}{H} v} \quad \otimes$$

shallow water

$$\dot{u} - fv = -g\eta_x$$

$$\dot{v} + fu = -g\eta_y$$

Vorticity $\dot{J} = v_x - u_y$

$$\dot{v}_x + f u_x + g v_{yx}$$

$$- \dot{u}_y + f v_y - g v_{xy} = 0$$

i.e. $\dot{J} + f(u_x + v_y) = 0$ (*)

with \oplus : $\dot{J} - f \frac{H_y}{H} v = 0$

Consider again $(Hu)_x + (Hv)_y = 0$

Idea: define streamfunction Ψ via

$$Hu = -\Psi_y, \quad Hv = \Psi_x$$

then continuity automatically fulfilled. (*) gives

$$0 = \partial_t \left[\partial_x \left(\frac{1}{H} \partial_x \Psi \right) + \partial_y \left(\frac{1}{H} \partial_y \Psi \right) \right] + \frac{f}{H} [(Hu)_x + (Hv)_y] \leftarrow$$

$\left(-\frac{f}{H} H_x u - \frac{f}{H} H_y v \right)$
 (product rule) (is 0)

$$\partial_t \left[\partial_x \left(\frac{1}{H} \partial_x \Psi \right) + \partial_y \left(\frac{1}{H} \partial_y \Psi \right) - \frac{f}{H^2} \partial_y H \partial_x \Psi \right] = 0$$

has solution

$$\Psi(x, y, t) = \sqrt{H(y)} \phi(y) e^{i(kx - \omega t)}$$

where ϕ obeys a new, simpler DGL.

eqn (10.12.4)

Trick: leave $\frac{H'}{2H}$ wherever possible

$$\frac{1}{H} \partial_t \partial_x^2 \Psi + \frac{1}{H} \partial_t \partial_y^2 \Psi - \frac{\partial_y H}{H^2} \partial_t \partial_y \Psi - \frac{f}{H} \frac{\partial_y H}{H} \partial_x \Psi = 0 \quad (*)$$

$$\begin{aligned} \partial_y \Psi &= \frac{\partial_y H}{2H^2} (\sqrt{H} \phi e^{i(kx - \omega t)}) + \frac{\partial_y \phi}{\phi} (\sqrt{H} \phi e^{i(kx - \omega t)}) \\ &= \left(\frac{H'}{2H} + \frac{\phi'}{\phi} \right) \Psi \end{aligned}$$

$$\begin{aligned} \partial_y \partial_y \Psi &= \partial_y \left(\frac{H'}{2H} + \frac{\phi'}{\phi} \right) \Psi + \left(\frac{H'}{2H} + \frac{\phi'}{\phi} \right) \partial_y \Psi \\ &= \left[\partial_y \left(\frac{\partial_y H}{2H} \right) + \frac{\phi \phi'' - \phi' \phi'}{\phi^2} \right] \Psi \\ &\quad + \left(\frac{\partial_y H}{2H} + \frac{\phi'}{\phi} \right) \left(\frac{\partial_y H}{2H} + \frac{\phi'}{\phi} \right) \Psi \end{aligned}$$

$$\begin{aligned} \text{in } (*) & \left\{ \frac{1}{H} (-k^2) (-i\omega) \Psi - \frac{i\omega}{H} \left[\partial_y \left(\frac{\partial_y H}{2H} \right) + \frac{\phi''}{\phi} - \left(\frac{\phi'}{\phi} \right)^2 \right. \right. \\ & \quad \left. \left. + \left(\frac{\partial_y H}{2H} \right)^2 + \frac{\partial_y H}{H} \frac{\phi'}{\phi} + \left(\frac{\phi'}{\phi} \right)^2 \right] \Psi \right. \\ & \quad \left. - \frac{2}{2} \frac{\partial_y H}{HH} (-i\omega) \left(\frac{H'}{2H} + \frac{\phi'}{\phi} \right) \Psi - \frac{f}{H} \frac{\partial_y H}{H} i k \Psi = 0 \right. \end{aligned}$$

$$- \frac{\omega}{H} \frac{\phi''}{\phi} - \frac{\omega}{H} \partial_y \left(\frac{\partial_y H}{2H} \right) - \frac{\omega}{H} \left(\frac{\partial_y H}{2H} \right)^2$$

$$\left(+ 2 \frac{\omega}{H} \left(\frac{\partial_y H}{2H} \right)^2 + \frac{k^2 \omega}{H} - \frac{f k}{H} \frac{\partial_y H}{H} \right) \Psi = 0 \quad \left| \cdot \frac{-H\phi}{\omega} \right.$$

(as so often)

$$\phi'' + \phi \left\{ \left(\frac{H'}{2H} \right)' - \left(\frac{H'}{2H} \right)^2 - k^2 + \frac{f k}{\omega} \frac{H'}{H} \right\} = 0$$

eqn p. 409 (10.12.6), roughly similar Pedlo p. 548

Specific shelf profile: $H = H_0 e^{2\lambda y}$

gives $-\ell^2\phi + 0\phi - \lambda^2\phi - k^2\phi + \frac{fk}{\omega} 2\lambda = 0$

$$\omega = \frac{2\lambda f k}{k^2 + \ell^2 + \lambda^2} \quad \text{eqn 10.12.9}$$

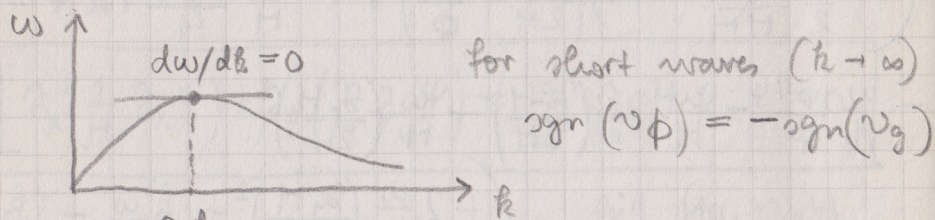
Very similar to Rossby wave dispersion relation, for similar physics: potential vorticity conservation, see below.

$$0 = \frac{d\omega}{dk} = (k^2 + \ell^2 + \lambda^2) 2\lambda f - 2\lambda f k \cdot 2k / \dots$$

$$= (\ell^2 + \lambda^2 - k^2) 2\lambda f / \dots$$

i.e. group speed zero if $k^2 = \ell^2 + \lambda^2$

$$\text{i.e. } \omega = \frac{2\lambda f \sqrt{\ell^2 + \lambda^2}}{2(\ell^2 + \lambda^2)} = \frac{\lambda f}{\sqrt{\ell^2 + \lambda^2}}$$

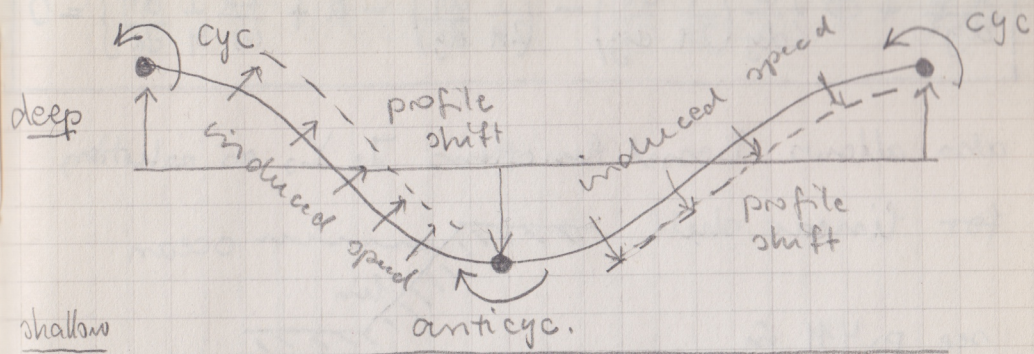


for short waves ($k \rightarrow \infty$)
 $\text{sgn}(\omega\phi) = -\text{sgn}(\omega_g)$

(figure similar to that for Rossby waves except for global sign $\omega = - \dots$)

for $v_g = 0$: Leewaves (mountain waves) due to topography

Physical mechanism as before



- 1) consider linear - straight vortex chain
- 2) sinusoidal perturbation causes vorticity change

$$V = \frac{f + J}{H} = \text{const (pot. vort.)}$$

i.e. if vortex goes deeper, $H \uparrow$, also $J \uparrow$: cyclonic

if vortex goes shallower, $H \downarrow$, also $J \downarrow$: anti-cyclonic

- 3) these cyclonic & anticyclonic changes in J cause a velocity field
- 4) that shifts the sinusoidal ("phase") profile of perturbation to the right

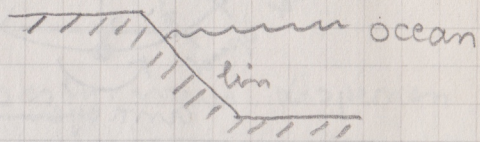
→ phase propagation with the coast & shallower water to the right in the north hemisphere, as usual.

the differential equation

$$\frac{d^2\phi}{dy^2} + \phi \left\{ \frac{d}{dy} \left(\frac{1}{2H} \frac{dH}{dy} \right) - \left(\frac{1}{2H} \frac{dH}{dy} \right)^2 - k^2 + \frac{\rho k}{\omega H} \frac{1}{dy} \right\} = 0$$

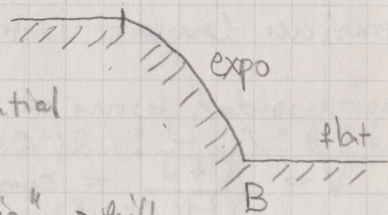
also allows Bessel functions J_0, Y_0 as solutions,

for linear shelf



see p. 411 in
Pedlosky

Other shelf profile:



turnover from exponential
to flat

"east coast of Australia" → gill